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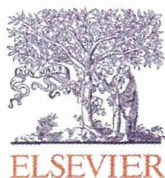
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Biomimetic hydration lubrication with various polyelectrolyte layers on cross-linked polyethylene orthopedic bearing materials

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ABSTRACT

Natural joints rely on fluid thin-film lubrication by the hydrated polyelectrolyte layer of cartilage. However, current artificial joints with polyethylene (PE) surfaces have considerably less efficient lubrication and thus much greater wear, leading to osteolysis and aseptic loosening. This is considered a common factor limiting prosthetic longevity in total hip arthroplasty (THA). However, such wear could be mitigated by surface modification to mimic the role of cartilage. Here we report the development of nanometer-scale hydrophilic layers with varying charge (nonionic, cationic, anionic, or zwitterionic) on cross-linked PE (CLPE) surfaces, which could fully mimic the hydrophilicity and lubricity of the natural joint surface. We present evidence to support two lubrication mechanisms: the primary mechanism is due to the high level of hydration in the grafted layer, where water molecules act as very efficient lubricants; and the secondary mechanism is repulsion of protein molecules and positively charged inorganic ions by the grafted polyelectrolyte layer. Thus, such nanometer-scaled hydrophilic polymers or polyelectrolyte layers on the CLPE surface of acetabular cup bearings could confer high durability to THA prosthetics.

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1. Introduction

The number of artificial hip and knee joints used for primary and revised hip replacement is increasing substantially every year all over the world [1]. Most patients who receive an artificial joint experience dramatic pain relief and rapid improvement in their daily activities as well as quality of life. The most popular artificial hip joint system is a bearing couple composed of polyethylene (PE; currently cross-linked PE or CLPE) and a cobalt–chromium–molybdenum (Co–Cr–Mo) alloy. However, osteolysis has emerged as a serious issue that limits the duration and clinical outcome of artificial hip joints [2,3]. Osteolysis is triggered by a host of inflammatory responses to PE wear particles originating from the interface [4], which undergo phagocytosis by macrophages and thus induce secretion of bone resorptive cytokines [5]. Hence, different combinations of bearing surfaces and improvements in

bearing materials have been studied with the aim of reducing the number of PE wear particles and extending the longevity of artificial hip joint [6–13]. However, few studies have explored methods to enhance the lubrication at the articular interface of artificial hip joints.

The bearing surfaces of a natural synovial joint are covered with a specialized type of hyaline cartilage, i.e., articular cartilage, which protects the joint interface from mechanical wear and facilitates a smooth motion of joints during daily activity [14,15]. The articular cartilage consists of chondrocytes, surrounding matrix macromolecules (e.g., proteoglycans, glycosaminoglycans, and collagens) and surface active phospholipids (SAPL; e.g., phosphatidylcholine derivatives). Due to their charge, they can trap water to maintain the water–fluid and electrolyte balance in the articular cartilages, which provides hydrophilicity and works as an effective boundary lubricant [16,17]. The fluid thin-film lubrication by the hydrated polyelectrolyte layer of articular cartilage is essential for the smooth motion of natural synovial joints. Given that learning from and mimicking nature is a widely successful theme in science and technology, it seems promising to

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investigate surface modification of bearing surfaces in artificial joints to mimic the role of cartilage.

Grafting of polymeric molecules onto a substrate through covalent bonding is a well-known method for modifying a polymer surface [18]. Grafting polymerization is mostly performed using either of the following methods: (1) surface-initiated graft polymerization, termed the “grafting from” method, in which monomers are polymerized from initiators or comonomers; and (2) adsorption of the polymer to the substrate, termed the “grafting to” method (i.e., dipping, cross-linking, and ready-made polymers reacting with the substrate) [19,20]. The former method has an advantage over the latter method in that it synthesizes a semi-dilute or high-density polymer brush [21].

In this study, we synthesized nanometer-scale hydrophilic layers on the CLPE surface of an artificial hip joint to reduce wear and avoid bone resorption. Our strategy is to modify the bearing surfaces of artificial joints with a hydrophilic polyelectrolyte layer to increase lubrication to levels that match articular cartilage under physiological conditions. Such nanometer-scale surface modification was accomplished using a photoinduced radical polymerization technique similar to the “grafting from” method; this approach renders only the surface of the CLPE substrate susceptible to modification and does not affect the bulk properties [22,23]. In addition, we investigated the effect of polyelectrolyte layers with various lubrication conditions on hydration lubrication [24] to realize the hydrophilicity and lubricity of the physiological joint surface. Such investigations are of great importance in the design of lubricated surfaces for artificial joints, and in better understanding the lubrication mechanisms of both natural and artificial joints. Here, we asked whether (1) the hydrophilic polymer or polyelectrolyte characteristics (i.e., nonionic, cationic, anionic, or zwitterionic) would affect the hydration- and friction-kinetics of the hydration layer and (2) the hydration lubrication characteristics of the polyelectrolyte layers might assure the durability of artificial hips.

2. Materials and methods

2.1. Chemicals

Benzophenone and acetone were purchased from Wako Pure Chemical Industries, Ltd. (Osaka, Japan). Oligo(ethylene glycol) methacrylate ($M_n = 360$; OEGMA) and 2-(dimethylamino)ethyl methacrylate (DMAEMA) were purchased from

Sigma–Aldrich Corp. (Saint Louis, MO, USA) and Tokyo Chemical Industry Co., Ltd. (Tokyo, Japan), respectively (Fig. 1A). 2-Methacryloyloxyethyl phosphate (MPA) was extracted from an aqueous suspension of Phosmer M solution (Unichemical Co., Ltd., Ikoma, Japan) with *n*-hexane (Kanto Chemical Co., Inc., Tokyo, Japan). 2-Methacryloyloxyethyl phosphorylcholine (MPC) was industrially synthesized by using the method reported by Ishihara et al. and supplied by NOF Corp. (Tokyo, Japan) [25].

2.2. Graft polymerization with various polyelectrolytes

A compression-molded PE (GUR1020 resin; Quadrant PHS Deutschland GmbH, Vreden, Germany) sheet stock was irradiated with a 50-kGy dose of gamma-rays in N_2 gas and annealed at 120 °C for 7.5 h in N_2 gas in order to facilitate cross-linking. CLPE specimens were then machined from this sheet stock after cooling.

These CLPE specimens were immersed in an acetone solution containing 10 mg/mL benzophenone for 30 s and then dried at room temperature in order to remove the acetone. Each monomer was dissolved in degassed pure water to obtain a 0.50-mol/L monomer aqueous solution, and the CLPE specimens coated with benzophenone were immersed in this solution. Photoinduced graft polymerization on the CLPE surface was performed using UV irradiation (UVL-400HA ultra-high pressure mercury lamp; Riko-Kagaku Sangyo Co., Ltd., Funabashi, Japan) with an intensity of 5 mW/cm² at 20 °C (DMAEMA) [26] or 60 °C (OEGMA, MPA, MPC) for 23–180 min (Fig. 1B); a filter (Model D-35; Toshiba Corp., Tokyo, Japan) was used to restrict the UV light to wavelengths of 350 ± 50 nm [27,28]. After polymerization, each of the poly(OEGMA) (POEGMA)-, poly(DMAEMA) (PDMAEMA)-, poly(MPA) (PMPA)-, and poly(MPC) (PMPC)-grafted CLPE specimens was removed, washed with pure water and ethanol, and dried at room temperature. These and untreated CLPE (as control) specimens were sterilized by with a 25-kGy dose of gamma-rays under N_2 gas [29].

2.3. Cross-sectional observation by transmission electron microscopy

A cross-section of the various polyelectrolyte-grafted layers on the CLPE surface with a 90-min photoirradiation time was observed under a transmission electron microscope (TEM). The specimens were embedded in epoxy resin, stained with ruthenium oxide vapor at room temperature, and finally sliced into ultra-thin films (approximately 100-nm-thick) by using a Leica Ultra Cut UC microtome (Leica Microsystems, Ltd., Wetzlar, Germany). The specimens of the various polyelectrolyte-grafted CLPE were pre-coated with a platinum–palladium thin film before embedding in epoxy resin to preserve the graft layer. A JEM-1010 electron microscope (JEOL, Ltd., Tokyo, Japan) was used for the TEM observations at an acceleration voltage of 100 kV.

2.4. Surface analysis of various polyelectrolyte-grafted CLPEs

The functional group vibrations of the various polyelectrolyte-grafted CLPE surfaces with a 90-min photoirradiation time were examined by Fourier-transform infrared (FT-IR) spectroscopy with attenuated total reflection (ATR) equipment. The FT-IR/ATR spectra were obtained using an FT-IR analyzer (FT/IR615; JASCO Co. Ltd., Tokyo, Japan) for 32 scans over the range 800–2000 cm⁻¹ at a resolution of 4.0 cm⁻¹.

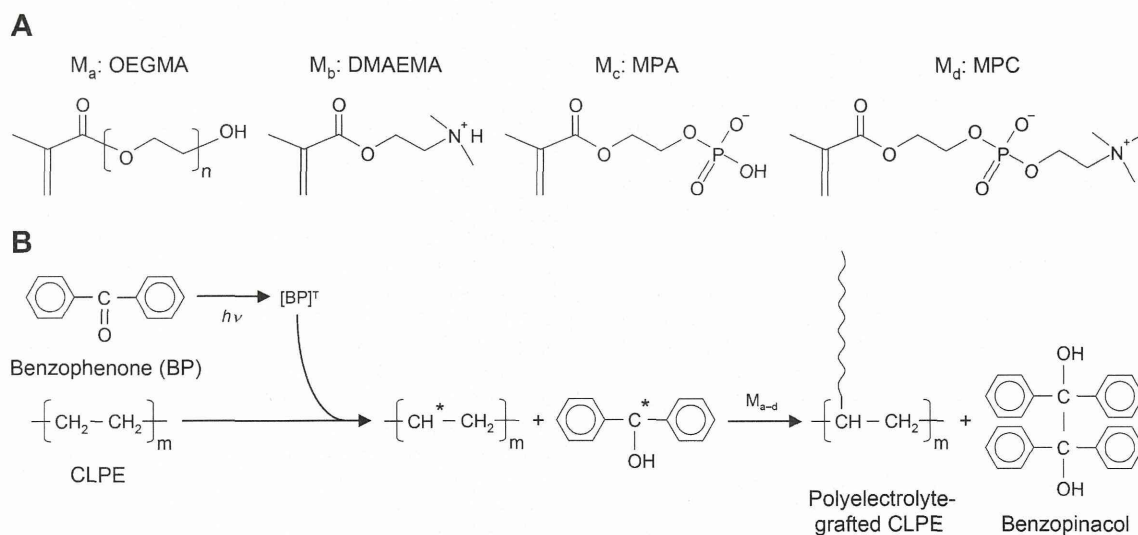


Fig. 1. Schematic illustration showing the preparation of various polyelectrolyte-grafted CLPE. (A) Monomers and (B) photoinduced graft polymerization.

The surface elemental conditions of the various polyelectrolyte-grafted CLPE surfaces with a 90-min photoirradiation time were analyzed by X-ray photoelectron spectroscopy (XPS). The XPS spectra were obtained using an XPS spectrophotometer (AXIS-HSi165; Kratos/Shimadzu Co., Kyoto, Japan) equipped with a 15-kV Mg-K α radiation source at the anode. The take-off angle of the photoelectrons was maintained at 90°. Five scans were taken for each sample.

The static-water contact angles on the various polyelectrolyte-grafted CLPE surfaces obtained at various photoirradiation times were measured by the sessile drop method using an optical bench-type contact angle goniometer (Model DM300; Kyowa Interface Science Co., Ltd., Saitama, Japan). Drops of purified water (1 μ L) were deposited on the various polyelectrolyte-grafted CLPE surfaces, and the contact angles were directly measured with a microscope 60 s after dropping. Measurements were repeated 15 times for each sample, and the average values were regarded as the contact angles.

2.5. Friction test

Friction tests were performed using a ball-on-plate machine (Tribostation 32; Shinto Scientific Co., Ltd., Tokyo, Japan) with various lubrication conditions. Each of the various polyelectrolyte-grafted CLPE surfaces was used to prepare six sample pieces. A 9-mm-diameter ball of Co–Cr–Mo alloy was prepared. The surface roughness (R_a) of the pin was less than 0.01 μ m, which is comparable to that of femoral head products. The friction tests were performed with a load of 0.98 N (contact stress roughly calculated by Hertzian theory is approximately 29 MPa), sliding distance of 25 mm, and a frequency of 1 Hz for a maximum of 100 cycles. The lubricants used were pure water at room temperature, acellular simulated body fluid (SBF, Kokubo solution, pH 7.4) with inorganic ion concentrations analogous to those found in human extracellular fluid at 37 °C [30], and a mixture of 25-vol% bovine serum at 37 °C. Before the friction tests, the specimens were pre-soaked in each lubricant for 24 h. The coefficient of dynamic friction for each specimen was determined by averaging five data points from the 100 (96–100) cycle measurements, and the average values for six sample pieces are reported as the mean coefficient of dynamic friction for each of the various polyelectrolyte-grafted CLPE surfaces.

2.6. Surface zeta potential measurement

The effective surface charge of the various polyelectrolyte-grafted CLPE surfaces was determined via an electrophoretic mobility method with an electrophoretic light-scattering spectrophotometer (ELS-800; Otsuka Electronics Co., Ltd., Osaka, Japan) equipped with a solid-plate sample cell. Before measurement, the specimens were equilibrated by soaking in a 0.01-mol/L sodium chloride aqueous solution for 1 h. The measurement was carried out in a 0.01-mol/L sodium chloride aqueous solution at 20 °C. Six samples for each of the various polyelectrolyte-grafted CLPE surfaces were prepared for the measurements, and the average values are reported as the surface zeta potential.

2.7. Characterization of protein adsorption by micro bicinchoninic acid method

The amount of protein adsorbed on the various polyelectrolyte-grafted CLPE surfaces was measured by the micro bicinchoninic acid (BCA) method. For each type of polyelectrolyte-grafted CLPE, ten sample pieces were prepared. Each specimen was immersed in Dulbecco's phosphate buffered saline (PBS; pH 7.4; ionic strength, 0.15 M; Immuno-Biological Laboratories Co., Ltd., Takasaki, Japan) for 1 h to equilibrate the polymer-grafted surface. The specimens were then immersed in bovine serum albumin (BSA; $M_w = 6.7 \times 10^4$; Sigma–Aldrich Corp., MO, USA) solution at 37 °C for 1 h. The protein solution was prepared at a BSA concentration of 4.5 g/L, i.e., 10% of the concentration of human plasma levels. Then, the specimens were rinsed five times with fresh PBS, immersed in a 1-mass% sodium dodecyl sulfate (SDS) aqueous solution, and shaken at room temperature for 1 h to detach completely the adsorbed BSA from the polymer-grafted CLPE surface. A protein analysis kit (micro BCA protein assay kit, #23235; Thermo Fisher Scientific Inc., IL, USA) based on the BCA method was used to determine the BSA concentration in the SDS solution, and

this value was used to determine the amount of BSA adsorbed on the polyelectrolyte-grafted CLPE surface.

2.8. Hip simulator wear test

A 12-station hip simulator (MTS Systems Corp., Eden Prairie, MN) with untreated CLPE and the various polyelectrolyte-grafted CLPE cups, each with inner and outer diameters of 26 and 52 mm, respectively, was used for the wear test according to the ISO standard 14242-3. Three sample pieces were prepared for each untreated CLPE and the various polyelectrolyte-grafted CLPE cups. A Co–Cr–Mo alloy ball with a diameter of 26 mm (K-MAX[®] HH-02; Japan Medical Materials Corp., Osaka, Japan) was used as the femoral component. A mixture of 25-vol% bovine serum was used as the lubricant, which was replaced every 0.5×10^6 cycles. Gait cycles were applied that simulated a physiological loading curve (Paul-type) with double peaks at 1793 and 2744 N (maximum contact stress roughly calculated by Hertzian theory is approximately 8 MPa) with a multidirectional (biaxial and orbital) motion at 1-Hz frequency. Gravimetric wear was determined by weighing the cups at intervals of 0.5×10^6 cycles. Load-soak controls ($n = 2$) were used to compensate for the fluid absorption by the specimens according to the ISO standard 14242-2. Testing was continued until a total of 3.0×10^6 cycles was completed. When the gravimetric method was used, the weight loss of the tested cups was corrected by subtracting the weight gain in the load-soak controls; however, this correction was not perfect because only the tested cups were continuously subjected to the motion and the load. In addition, after 3.0×10^6 cycles of the hip simulator test, the volumetric wear of the cups was measured using a three-dimensional coordinate measurement machine (BHN-305; Mitsutoyo Corp., Kawasaki, Japan) and reconstructed using three-dimensional modeling software (Imageware; Siemens PLM Software Inc., Plano, TX).

Wear particles were observed under a field emission scanning electron microscope (FE-SEM). The wear particles were isolated from the bovine serum solution used as lubricant in the hip simulator wear tests. To isolate the wear particles, the lubricant was incubated in a 5-mol/L sodium hydroxide solution for 3 h at 65 °C to digest adhesive proteins that were degraded and precipitated. To avoid artifacts, the contaminating proteins were removed by extraction with solutions having several densities: sugar solution, 1.20 g/cm³ and 1.05 g/cm³; and isopropyl alcohol solution, 0.98 g/cm³ and 0.90 g/cm³. This was followed by centrifugation at 25,500 rpm for 3 h at 5 °C (himac CP 70MX; Hitachi Koki Co., Ltd, Tokyo, Japan). The collected solution was sequentially filtered through a 0.1- μ m membrane filter, and the membrane was observed directly under an FE-SEM (JSM-6330F; JEOL DATUM Co., Ltd, Tokyo, Japan) at an acceleration voltage of 20 kV after gold deposition.

2.9. Statistical analysis

The mean values of the groups (untreated and various polyelectrolyte-grafted CLPE) were compared by one-factor analysis of variance (ANOVA) and the significance of differences in the static-water contact angle (static-water contact angle measurement), dynamic friction coefficient (ball-on-plate friction test), surface zeta potential (surface zeta potential measurement), and amount of adsorbed BSA (protein adsorption measurement by micro BCA method) were determined by post-hoc testing using Bonferroni's method. The statistical significance of gravimetric wear (hip simulator test) was judged by the Student's *t*-test. All statistical analyses were performed using add-on software (Statcel 2; OMS publishing Inc., Tokorozawa, Japan) for a computerized worksheet (Microsoft Excel[®] 2003; Microsoft Corp., Redmond, WA).

3. Results

As shown in the cross-sectional TEM images in Fig. 2, all graft polymerization processes afforded a uniform grafted polyelectrolyte layer on the CLPE surface with almost constant thicknesses of 100–150 nm.

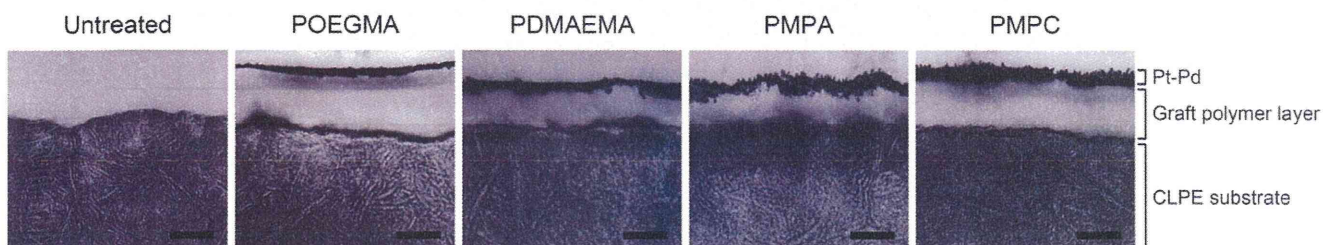


Fig. 2. Cross-sectional TEM images of untreated CLPE and various polyelectrolyte-grafted CLPE samples obtained with a 90-min photoirradiation time. Bar: 100 nm.

Fig. 3 shows the FT-IR/ATR and XPS spectra of the untreated CLPE and various polyelectrolyte-grafted CLPE samples subjected to photoirradiation for a 90 min. The FT-IR/ATR spectra after grafting contained new absorption peaks at 1720 cm^{-1} (C=O); 1090 and 1040 cm^{-1} (ether or carbohydrate group); 1140 and 960 cm^{-1} (protonated or carbonated ammonium group); and 1240 , 1080 , and 970 cm^{-1} (phosphate group) for each of the polyelectrolyte-grafted CLPE samples. These peaks are chiefly attributed to the graft polymer on each CLPE surface. The XPS spectra of the binding energy region of the nitrogen (N) and/or phosphorous (P) electrons showed peaks for the PDMAEMA-, PMPA-, and PMPC-grafted CLPE samples, whereas peaks were not observed for untreated CLPE and the POEGMA-grafted CLPE samples. The peaks at 400 and 403 eV are attributed to N–H, $-\text{NH}^+(\text{CH}_3)_2$, and $-\text{N}^+(\text{CH}_3)_3$, respectively. The peak at 134 eV is attributed to the phosphate groups. These peaks indicate the presence of a dimethylamino group in the DMAEMA units, phosphonoxy group in the MPA units, and phosphorylcholine group in the MPC units. Overall, these results from TEM observation, FT-IR/ATR, and XPS analyses indicate that the various polyelectrolytes were successfully grafted on the CLPE surface.

Next, as shown in Fig. 4, the static-water contact angle was 95° for untreated CLPE and this value decreased as the photoirradiation time increased. Thus, clearly, the photoirradiation time affected the hydration-kinetics of the polyelectrolyte graft chains. However, the decrease (or decrease rate) of the static-water contact angle differed for each of the polyelectrolyte-grafted CLPE surfaces. Nevertheless, after photoirradiation for more than 90 min (45 min for POEGMA-grafted CLPE), the static-water contact angles of all polyelectrolyte-grafted CLPE samples reached the lowest values of 20° – 60° .

Fig. 5 shows the coefficient of dynamic friction of polyelectrolyte-grafted CLPE samples obtained with a 90-min photoirradiation time in various lubricants. Control measurements

were carried out in water as the lubricant. From the figure, we see that the coefficients of dynamic friction for the polyelectrolyte-grafted CLPE samples were 0.01 – 0.05 , representing a 40% – 85% reduction compared with untreated CLPE. A calcification-like mineralized surface morphology was observed on the PMPA-grafted CLPE surface after SBF pre-soaking for 24 h before the friction test. The coefficient of dynamic friction of the POEGMA- and PMPC-grafted CLPE surfaces did not differ significantly ($p > 0.05$) between lubricants. The coefficient of dynamic friction of PMPC-grafted CLPE was significantly ($p < 0.01$) lower than that of POEGMA-grafted CLPE under each lubrication condition; the same relation was found for the static-water contact angles of the two types of polyelectrolyte-grafted CLPE surfaces. In contrast, the coefficient of dynamic friction of the PDMAEMA- and PMPA-grafted CLPE surfaces increased drastically ($p < 0.01$) in SBF and BS, respectively. In addition, the untreated CLPE also showed increased friction in BS lubricant compared with that in water.

Fig. 6 shows the surface zeta potential and the amount of BSA adsorbed on the untreated CLPE and the various polyelectrolyte-grafted CLPE samples with a 90-min photoirradiation time. As seen in the figure, the surface zeta potential of the untreated CLPE and the POEGMA- and PMPC-grafted CLPE surfaces with nonionic and zwitterionic grafted polymer layers was close to zero (Fig. 6A). In contrast, that of PDMAEMA-grafted CLPE with cationic grafted polymer layers was 50.6 mV , which is strongly positive, and that of PMPA-grafted CLPE with anionic grafted polymer layers was -32.5 mV , which is strongly negative. The amount of adsorbed BSA on the POEGMA-, PMPA-, and PMPC-grafted CLPE surfaces with nonionic, anionic, and zwitterionic grafted polymer layers significantly ($p < 0.01$) decreased (Fig. 6B). In contrast, that of PDMAEMA-grafted CLPE with a cationic grafted polymer layer increased ($p < 0.01$).

Fig. 7 shows how the polyelectrolyte hydrated layer characteristics affected the durability of artificial hips. Three-dimensional

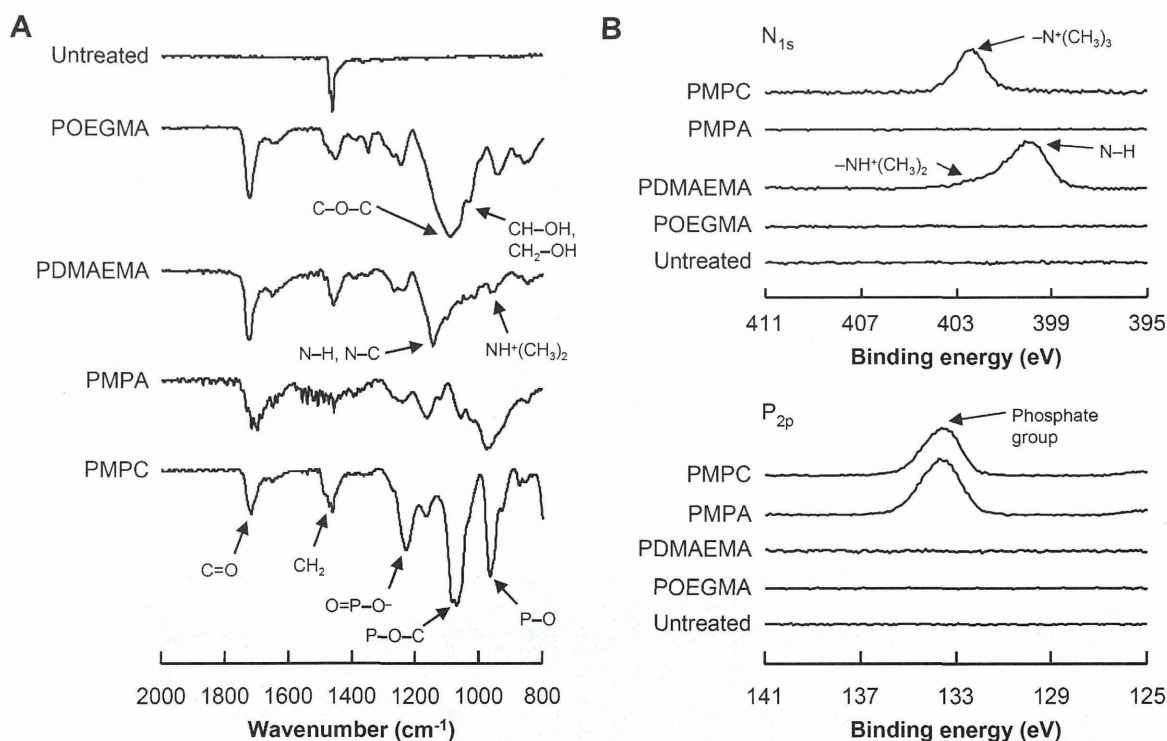


Fig. 3. (A) FT-IR/ATR and (B) XPS spectra of untreated CLPE and various polyelectrolyte-grafted CLPE samples obtained with a 90-min photoirradiation time.

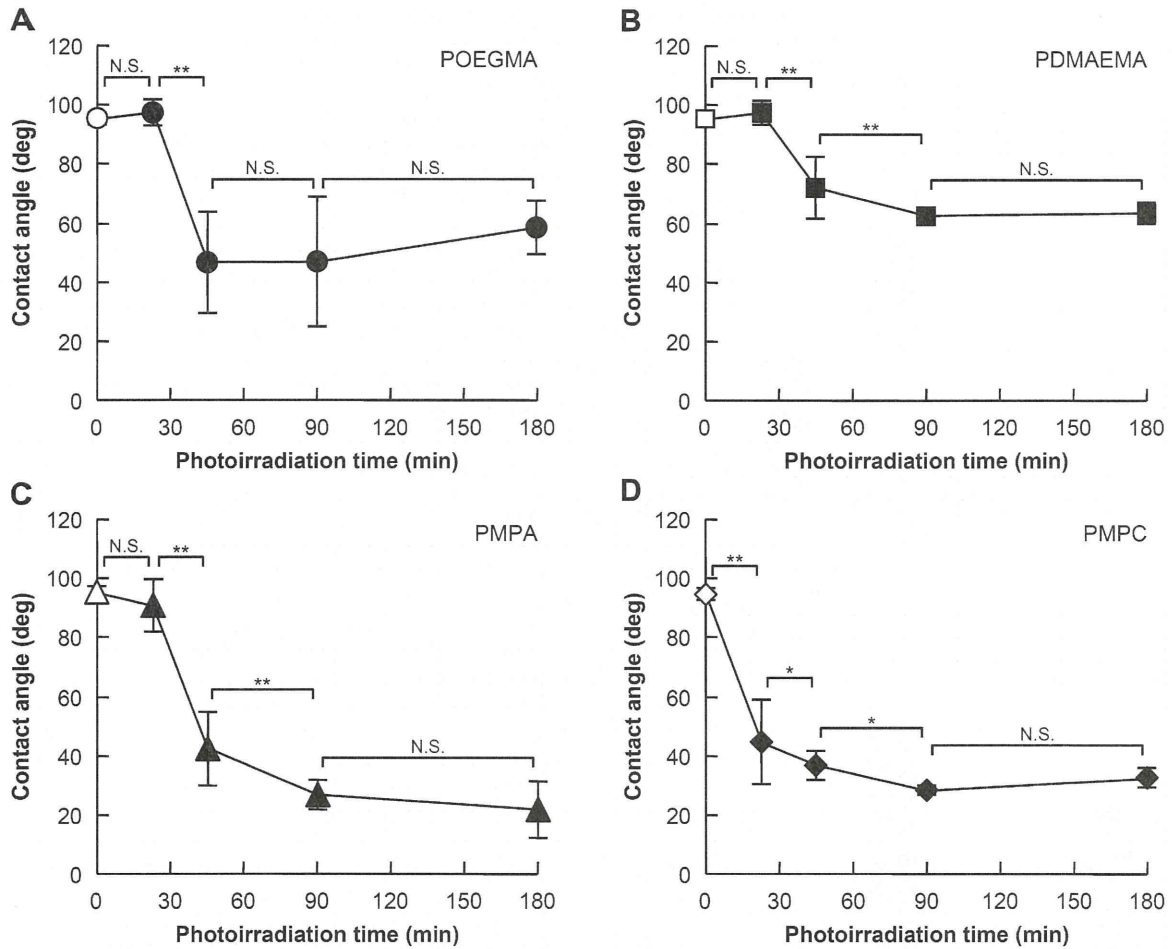


Fig. 4. Static-water contact angle on various polyelectrolyte-grafted CLPE surfaces as a function of the photoirradiation time. (A) POEGMA-grafted, (B) PDMAEMA-grafted, (C) PMPA-grafted, and (D) PMPC-grafted CLPE. Data are expressed as means \pm standard deviations. * Indicates $p < 0.05$, ** indicates $p < 0.01$, and N.S. indicates no statistical difference.

coordinate measurements with the polyelectrolyte-grafted CLPE cups revealed little to no detectable volumetric wear, although substantial volumetric wear was detected in the untreated CLPE (Fig. 7A). The wear particles of untreated CLPE and polyelectrolyte-

grafted CLPE cups after $0.5\text{--}1.0 \times 10^6$ cycles of the hip simulator test, as characterized by FE-SEM, were predominantly sub-micrometer-sized granules (Fig. 7B). In all cases, the morphologies of the wear particles exhibited no remarkable difference. However, remarkably fewer wear particles were found for POEGMA- and PMPC-grafted CLPE cups than for untreated CLPE cups.

Fig. 8 shows the time course of gravimetric wear of the various polyelectrolyte-grafted CLPE cups during the hip simulator test. PDMAEMA-, POEGMA-, and PMPC-grafted CLPE cups were found to undergo significantly less gravimetric wear than untreated CLPE cups. These gravimetric wear results support the volumetric wear images in Fig. 7A. Furthermore, POEGMA- and PMPC-grafted CLPE cups showed a slight, gradual increase in weight during the hip simulator test. This is partially attributable to greater fluid (e.g., water, proteins, and lipids) absorption in the tested cups than in the load-soak controls. Note that when using the gravimetric method, the weight loss of the tested cups was corrected by subtracting the weight gain in the load-soak controls; however, this correction is not perfect because only the tested cups are continuously subjected to motion and load.

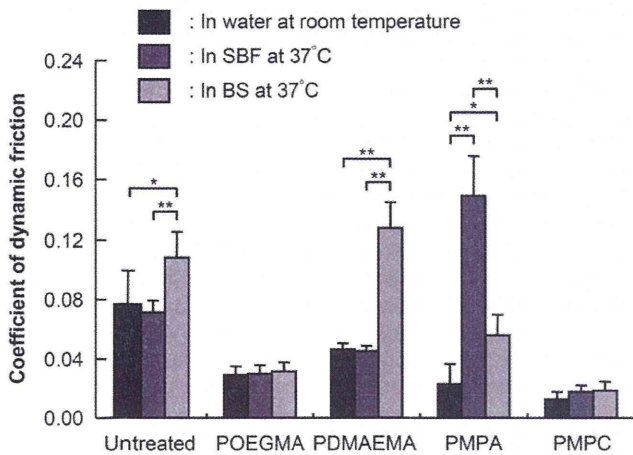


Fig. 5. Coefficient of dynamic friction of polyelectrolyte-grafted CLPE samples obtained with a 90-min photoirradiation time in the ball-on-plate friction test under various lubrication conditions. Data are expressed as means \pm standard deviations. * Indicates $p < 0.05$, ** indicates $p < 0.01$, and N.S. indicates no statistical difference.

4. Discussion

In natural synovial joints under physiological conditions, fluid film lubrication by the hydrated layer is essential for the smooth

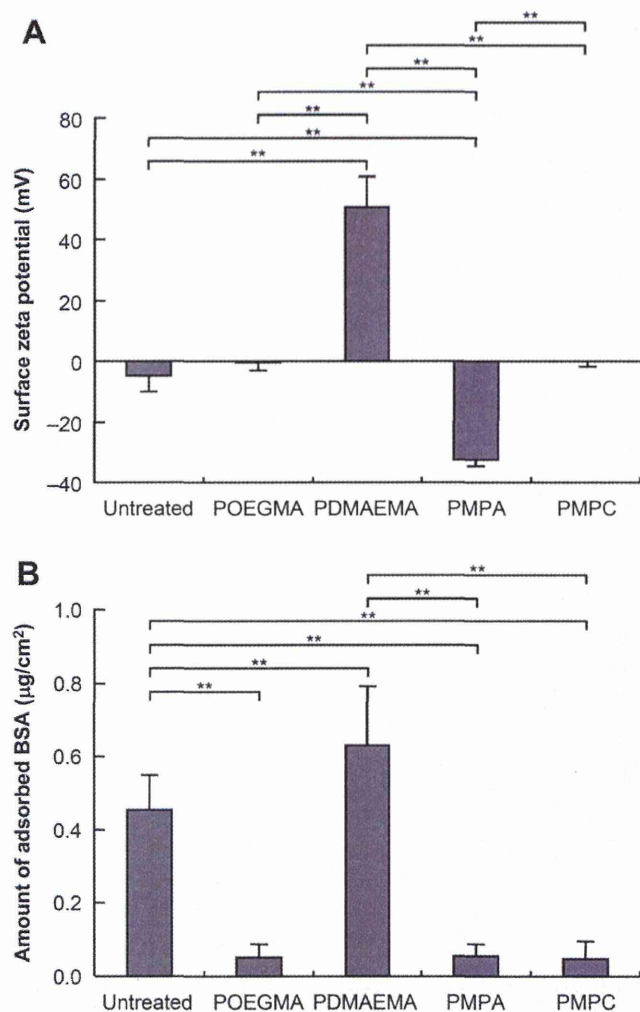


Fig. 6. Surface zeta potential and the amount of adsorbed BSA for untreated CLPE and the various polyelectrolyte-grafted CLPE samples with a 90-min photoirradiation time. Data are expressed as means \pm standard deviations. ** Indicates $p < 0.01$.

motion of joints [31], and a nanometer-scaled hydrated polyelectrolyte layer that covers the joint cartilage surface provides hydrophilicity and works as an effective boundary lubricant [14–17]. Hence, grafting a cartilage-like hydrophilic polymer layer onto the bearing surface of an artificial joint may afford the same hydrophilicity and lubricity of the physiological joint surface [32]. With this viewpoint, we specifically investigated whether (1) the hydrophilic polymer or polyelectrolyte characteristics would affect the hydration- and friction-kinetics of the hydration layer and (2) the characteristics of hydration lubrication [24] of polyelectrolyte layers might assure the durability of artificial hips.

The results of the TEM, FT-IR/ATR, and XPS analyses confirmed successful synthesis of nanometer-scale hydrophilic layers with varying charge (nonionic/neutral, cationic, anionic, or zwitterionic properties) on a CLPE surface. The results also showed that the hydrophilicity of each of the various polyelectrolyte-grafted CLPE surfaces gradually increased with the photoirradiation time, as previously reported (Fig. 4) [23]. To obtain a uniform graft layer on a CLPE surface, the photoirradiation time during graft polymerization must be controlled [27]. Controlled 100-nm-thick, uniform graft layers with varying charge are essential for a proper comparison of friction and wear performance under various lubricant conditions.

Specifically, the results of the present study show that the charge (nonionic, cationic, anionic, or zwitterionic) of the graft layer affects the hydration- and friction-kinetics of the CLPE bearing surface; the coefficient of dynamic friction in ball-on-plate friction test with a water lubricant depends on the hydrophilicity (static-water contact angles) as shown in Figs. 4 and 5. All of the polyelectrolyte-grafted CLPE surfaces exhibited considerably higher lubricity than the untreated CLPE surface in a water lubricant. This is because the water molecules in the hydration layers of the hydrophilic polymer or polyelectrolytes act as very efficient lubricants [32,33]. However, in other lubricant conditions, the polyelectrolyte-grafted CLPE surfaces with cationic and anionic polymer layer exhibited significantly different characteristics compared with neutral hydrophilic polymer- or zwitterionic polyelectrolyte-grafted CLPE surfaces, even though all showed high hydrophilicity.

The PDMAEMA-grafted CLPE samples exhibited a higher coefficient of dynamic friction in the BS lubricant containing proteins (e.g., albumin, globulin) than in water or SBF lubricants in the ball-on-plate friction test [34]. PDMAEMA has a positively charged $-\text{NH}^+(\text{CH}_3)_2$ group at neutral pH, which in turn attracts negatively charged molecules (e.g., albumin molecules have negatively charges at neutral pH) (Fig. 6). This implies that the existence of protein molecules at the bearing interface increases the resistance to sliding motion. Since protein is adsorbed on the Co–Cr–Mo alloy counterface [35,36], the high resistance to sliding motion is interpreted as being the result of higher adhesive interaction or interpenetration of the adsorbed protein films formed on both PDMAEMA-grafted CLPE and Co–Cr–Mo alloy surfaces. However, the PDMAEMA-grafted CLPE cups exhibited high wear resistance in the hip simulator test at high load, despite the high coefficient of dynamic friction in the ball-on-plate friction test in the BS lubricant. This may be because the adsorbed protein film from the BS lubricant is squeezed out of the bearing interface at high load [37].

In contrast, the PMPA-grafted CLPE surfaces exhibited considerably poor lubricity in the ball-on-plate friction test with an SBF lubricant. The chemical structure of the negatively charged PMPA is characterized by the presence of a large number of trap sites for positively charged inorganic ions. Hence, the poor lubricity of PMPA-grafted CLPE surfaces is interpreted as being due to shrinkage or bridging of negatively charged polyelectrolyte chains, which reduced the mobility of the chains in a solution containing positively charged inorganic ions [32–34]. In a previous study, Kato et al. reported that PMPA-grafted poly(ethylene terephthalate) surfaces induced hydroxyl apatite deposition in SBF, mimicking biological mineralization [38]. In this study, a similar phenomenon was observed as the PMPA-grafted CLPE surfaces exhibited calcification-like mineralization after pre-soaking in SBF for 24 h before the friction test. (The chemical composition of the mineralized thin layer on the PMPA-grafted CLPE surfaces could not be detected by thin film X-ray diffraction analysis.) The BS lubricant in this hip simulator test contained not only protein molecules but also inorganic ions. Further, during the 3.0×10^6 cycles of the hip simulator test, the test cups were soaked in the BS lubricant for over 30 days. It is therefore thought that the negatively charged PMPA in turn attracts only positively charged inorganic ions and repels the negatively charged molecules; the PMPA-grafted CLPE cups exhibited higher wear than the other polyelectrolyte-grafted CLPE cups due to abrasive wear by the mineralized hardened surface layer [39].

The POEGMA- and PMPC-grafted CLPE cups exhibited high wear resistance in the hip simulator tests (Figs. 7 and 8) as well as low coefficients of dynamic friction in the ball-on-plate friction tests (Fig. 5). In particular, the highly hydrated surface layer of PMPC-grafted CLPE provided extremely efficient lubrication under all

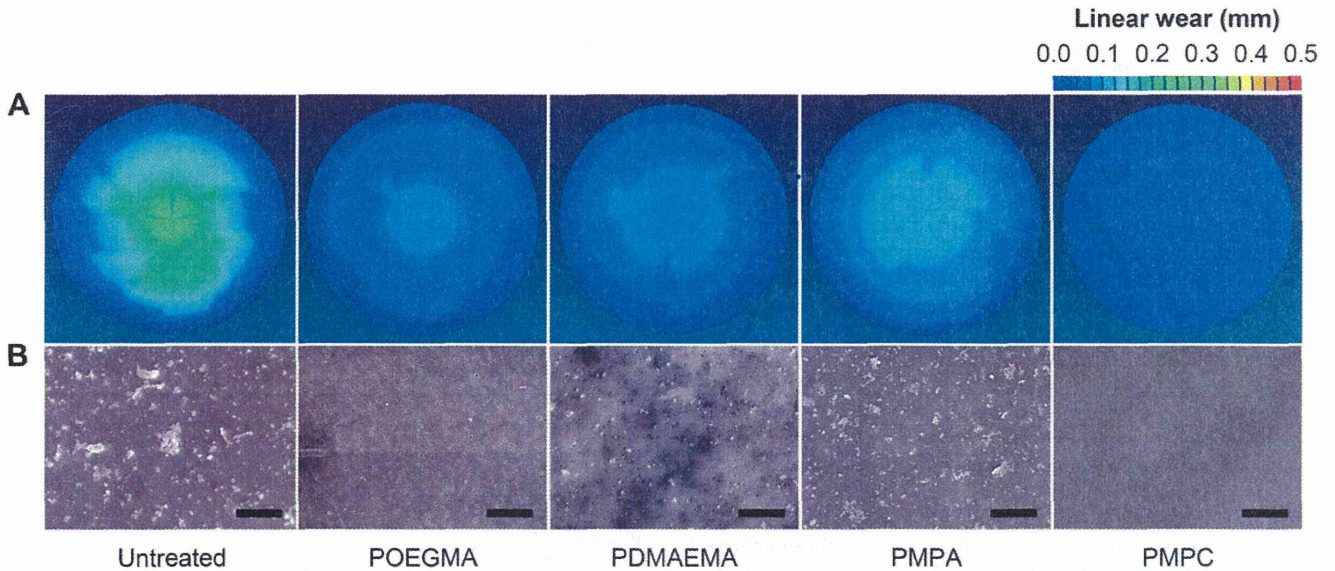


Fig. 7. Analysis of various polyelectrolyte-grafted CLPE cups after the hip simulator test. (A) Three-dimensional coordinate measurements of various polyelectrolyte-grafted CLPE cups and (B) SEM images of wear particles isolated from lubricants of the hip simulator test. Scale bar indicates 5 μm .

conditions. Moreover, the zeta potential of the PMPC-grafted CLPE surface was close to zero because the ionic group in the MPC unit forms an inner salt and the electrostatic effects are diminished. Therefore, the zwitterionic grafted polymer layers attract water molecules only, and repel the protein molecules (Fig. 6B) and positively charged inorganic ions. This characteristic is the same as that of the nonionic grafted polymer layers. Chen et al. reported that the water molecules adsorbed on the surface of highly hydrophilic polyzwitterionic (i.e., PMPC) brushes act as lubricants to reduce the interaction between the brushes and the counter-surface [40]. Recent efforts to identify hydrophilic polymers or polyelectrolytes have focused on nanotribological studies of surface-attached molecules, seeking to emulate those at the cartilage surface [32,41,42]. However, the above results for PDMAEMA- and PMPA-grafted CLPE in the hip joint simulator tests demonstrate

that the mechanism of action of the polyelectrolyte-grafted layer cannot be explained simply in terms of fluid film lubrication. Therefore, we believe that the primary mechanism underlying the low friction and high wear resistance is the high level of hydration of the polyelectrolyte layer, such as the zwitterionic PMPC-grafted layer; water molecules in the hydration layers act as very efficient lubricants [32,42,43]. The secondary mechanism is attributed to a repulsion of protein molecules by the positively charged inorganic ions of the polyelectrolyte layer in a synovial fluid, which may reduce the adhesive interaction or interpenetration between opposing Co–Cr–Mo alloy surfaces or adsorbed protein films on the Co–Cr–Mo alloy [8,40].

After 3.0×10^6 cycles of the hip simulator test, the POEGMA-, PDMAEMA-, and PMPC-grafted CLPE cups show a greater than 97% reduction in steady wear rate (-1.82 – 0.12 mg/ 10^6 cycles) compared with untreated CLPE (Fig. 8). This suggests the approach may be promising for extending the longevity of THA prosthetics [44]. To explain this we assume that the hydrated bearing surface of the artificial joint modified with PMPC exhibited fluid film lubrication (i.e., hydration lubrication [24,45]) and suggest this artificial hip mimics the cartilage or SAPL layer on the cartilage in natural joints [23]. Although the PMPC layer has no direct analog to the cartilage surface containing SAPL, the results of the present study underline the possible importance at such surfaces of highly hydrated macromolecules in the chondroprotective and lubrication roles.

The POEGMA- and PMPC-grafted CLPE cups did not lose weight during the hip simulator test; instead, they gained weight even after correction for water absorption in the load-soak control, suggesting an underestimation of the load-soak control, as previously reported [12,46]. The cups showed comparable weight gains after 3.0×10^6 cycles, irrespective of the presence or absence of the POEGMA- and PMPC-graft layers, confirming that the weight gain was the result of the water absorbed by the cup material (i.e., the CLPE substrate) and not the result of retention of extraneous materials on the surface POEGMA- and PMPC-graft layers. These cups decreased the amount of wear particles isolated from the lubricants. Because wear particles from POEGMA- and PMPC-graft CLPE surfaces were hardly observed as a result of their extremely

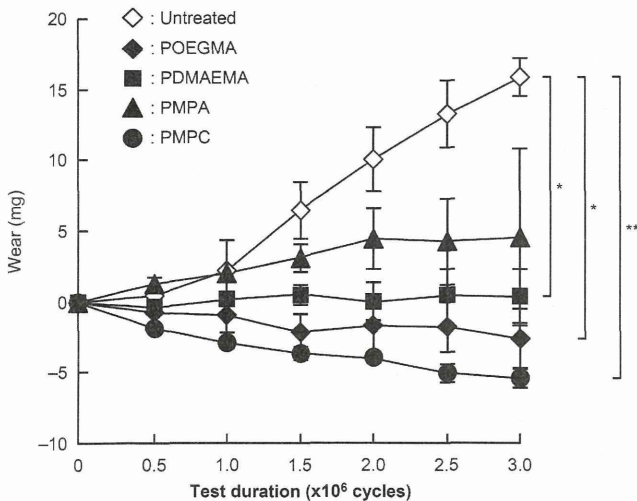


Fig. 8. Time course of gravimetric wear of various polyelectrolyte-grafted CLPE cups during the hip simulator test. Data are expressed as means \pm standard deviations. * Indicates $p < 0.05$, ** indicates $p < 0.01$ as compared with an untreated CLPE cup.